



## Preparation of mullite whiskers reinforced SiC/Al<sub>2</sub>O<sub>3</sub> composites by microwave sintering

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### Abstract

Mullite whiskers reinforced SiC/Al<sub>2</sub>O<sub>3</sub> composites were prepared by microwave sintering in a microwave chamber with TE<sub>666</sub> resonant mode. Original SiC particles were coated with SiO<sub>2</sub> using sol-gel processing and mixed with Al<sub>2</sub>O<sub>3</sub> particles. Mullite was formed in the reaction between SiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub>. The isostatically pressed cylindrical pellets were sintered from 1350 °C to 1600 °C for 30 min. Physical and chemical responses were investigated by detecting changes in reflected power during the microwave sintering process. XRD was carried out to characterize the samples and showed that mullite could be formed at 1200 °C. Bridging of mullite whiskers between Al<sub>2</sub>O<sub>3</sub> and SiC particles was observed by SEM and is due to a so-called local hot spot effect, which was the unique feature for microwave sintering. The optimized microwave sintering temperature was 1500 °C corresponding to the maximum amount of mullite whiskers within SiC/Al<sub>2</sub>O<sub>3</sub> composites. The high electro-magnetic field enhanced the decomposition of mullite at higher temperatures above 1550 °C. The mechanical properties of mullite whiskers reinforced SiC/Al<sub>2</sub>O<sub>3</sub> composites are much better than the SiC/Al<sub>2</sub>O<sub>3</sub> composites without mullite whiskers.

**Keywords:** microwave sintering, SiC/Al<sub>2</sub>O<sub>3</sub> composites, mullite whiskers, bridging, local hot spot effect

### I. Introduction

Al<sub>2</sub>O<sub>3</sub>-based composites have been widely used in mechanical, chemical engineering, metallurgy, military and electronic fields because of their excellent refractoriness, low electrical conductivity, oxidation resistance, good chemical stability [1–4]. Most researches have focused on particle-dispersed Al<sub>2</sub>O<sub>3</sub> composites to improve mechanical properties [3,5]. SiC, ZrO<sub>2</sub>, TiN, TiO<sub>2</sub>, Y<sub>2</sub>O<sub>3</sub>, and some metal particles (Cr) are good candidates as reinforcement for Al<sub>2</sub>O<sub>3</sub> composites [6–13]. SiC/Al<sub>2</sub>O<sub>3</sub> composites have recently received considerable attention due to their superior properties such as high modulus, high hardness, and good high-temperature strength [2]. Nevertheless, the oxidation of SiC into SiO<sub>2</sub> at high temperatures limits the application of SiC/Al<sub>2</sub>O<sub>3</sub> composites. Such problem could be suc-

cessfully solved by coating SiO<sub>2</sub> on SiC particles which facilitates the reaction between SiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> to form mullite at high temperature. Mullite shows comparable thermal expansion coefficient and excellent chemical compatibility with SiC [14,15]. Mullite reinforced SiC/Al<sub>2</sub>O<sub>3</sub> composites are promising materials in the field of engineering ceramics due to their excellent high temperature mechanical properties and well resistance toward chemical attack [16–20]. Pressureless sintering or hot pressing are traditionally carried out to prepare mullite reinforced SiC/Al<sub>2</sub>O<sub>3</sub> composites [16,19]. The sintering temperature is very high and the mullite formation by the reaction between SiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> could not be controlled. Microwave sintering as a new heating method has presently been investigated to prepare oxides and other composites [21–23]. The unique heating behaviour helps to reduce temperature and time for sintering, as well as to improve microstructure of the samples [24–26].

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In this study, microwave sintering is carried out to prepare mullite whiskers reinforced SiC/Al<sub>2</sub>O<sub>3</sub> composites. Physical and chemical responses during the microwave sintering process are investigated. Mechanisms on the formation of mullite are analysed.

## II. Experimental

$\alpha$ -SiC particles with average diameter of  $\sim 10\ \mu\text{m}$  were commercially available from Henan Haixu Abrasives Co. Ltd.  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> particles ( $\sim 1\ \mu\text{m}$ , with the purity of 99.7%) were prepared by conventional pyrolysis of aluminium hydroxide precursor at 1300 °C for 30 min. A sol-gel method was carried out to coat SiO<sub>2</sub> on SiC particles through the hydrolysis of tetraethyl orthosilicate, the SiO<sub>2</sub>/SiC volume ratio was 1:5. During the coating process, SiC particles were suspended in distilled water and ultrasonicated for 30 min to break down agglomerates. The pH value of the suspension was adjusted at about 2 by HCl. Tetraethyl orthosilicate in alcohol solution was then added to the suspension with stirring for 3 h. Then NH<sub>3</sub>·H<sub>2</sub>O was mixed into the suspension and the pH value was controlled at 10–11. The

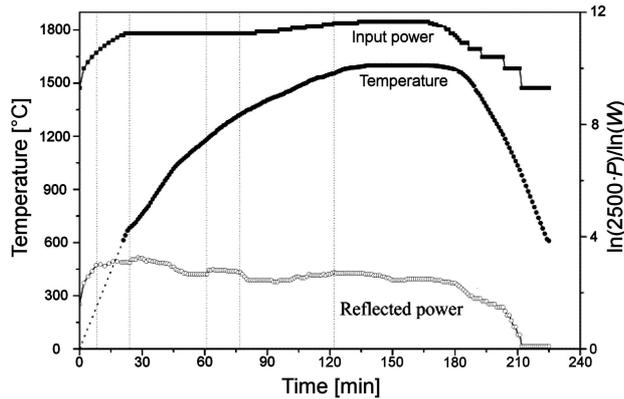


Figure 1. Heating profile for composites preparation and corresponding changes in input and reflected power

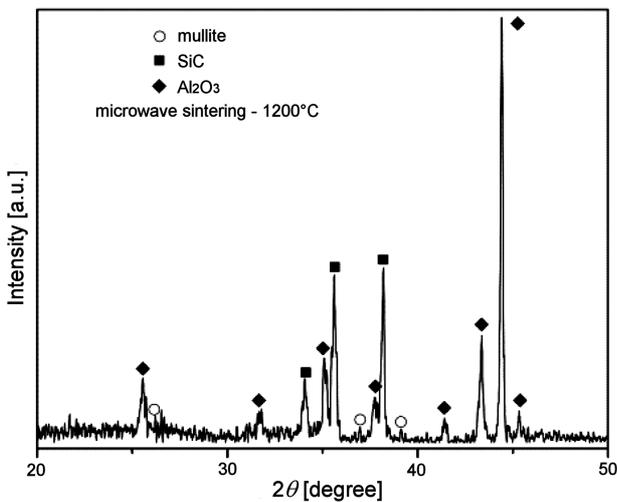


Figure 2. XRD patterns of samples prepared by microwave sintering at 1200 °C for 20 min

gel of SiO<sub>2</sub>/SiC composite precursor was formed in a few minutes. Then the coated composite particles were mixed with  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> particles in the volume ratio 1:1. Mullite was expected to form by the reaction between SiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> during microwave sintering.

The mixed powders were uniaxially pressed into a cylindrical pellets ( $\phi = 30\ \text{mm}$  and  $H = 4\ \text{mm}$ ) at 10 MPa for 1 min. After isostatically pressing at 100 MPa for 1 min, the prepared green cylindrical pellets were sintered in a microwave chamber with resonant mode of TE<sub>666</sub> (WXD20S-07, China Nanjing Sanle Microwave equipment). The frequency of microwave was 2.45 GHz with a maximum input power of 10 kW. The temperature was monitored by an infrared radiation thermometer (OI-T6I2-B-1-type, GOID SUN, USA) with initial display temperature of 610 °C. An insulation structure based on a hybrid heating mode was well designed with wall of porous mullite plate, fillings of mullite fibres and aided heaters of SiC rods. Heating rate was arbitrarily controlled by tailoring the input power. Changes in reflected power versus temperature were detected. The selected sintering temperature was 1350 °C, 1400 °C, 1450 °C, 1500 °C, 1550 °C and 1600 °C for 30 min with a heating rate of 15 °C/min, respectively.

Phases of the samples were detected by X-ray diffraction (XRD; XD-3, Beijing Purkinje General Instrument Co. Ltd.). Microstructure of samples was observed by field emission scanning electron microscopy (FESEM; JEOL JSM-6700F, Japan) equipped with energy dispersive spectroscopy analysis (EDS). The samples for SEM analysis were coated with a Pt layer by a vacuum sputtering.

## III. Results and discussion

Figure 1 illustrates time dependent changes in input power and reflected power together with instantaneous temperature for SiC/Al<sub>2</sub>O<sub>3</sub> composites sintered at 1600 °C. Six consecutive heating stages can be distinguished, from which physical and chemical responses during the microwave sintering process could be revealed. At the initial heating stage, microwave is primarily absorbed by SiC aided heaters and SiC particles within SiC/Al<sub>2</sub>O<sub>3</sub> samples since the dielectric loss of Al<sub>2</sub>O<sub>3</sub> particles is very low at low temperature [27,28]. The heat generated by SiC particles within SiC/Al<sub>2</sub>O<sub>3</sub> samples is isolated and gives rise to a so-called local hot spot effect during the microwave sintering [29–32]. The reflected power increases synchronously with input power, as indicated before 8 min (estimated 200 °C). It does not change obviously with the increasing input power from 8 min to 25 min. This indicates the developed microwave absorbing ability due to the increases in dielectric loss of SiC as the temperature rises. At about 25 min ( $\sim 700\ \text{°C}$ ), the reflected power increases instantly. It implies that surface oxidation of SiC aided heaters initiates formation of SiO<sub>2</sub>, which lowers microwave absorption ability. The reflected power keeps

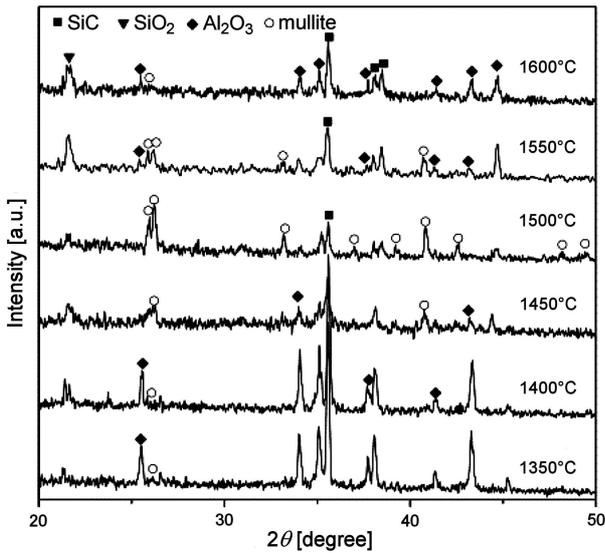


Figure 3. XRD patterns of SiC/Al<sub>2</sub>O<sub>3</sub> composites sintered at different temperature for 30 min

increasing until ~30 min, indicating that the oxidation finishes after 30 min. The subsequent decrease in the reflected power appears due to the improved conductivity of SiC aided heaters and SiC particles within SiC/Al<sub>2</sub>O<sub>3</sub> greens, as well as the increased dielectric loss of Al<sub>2</sub>O<sub>3</sub> at higher temperature. The reflected power rises after 62 min (~1200 °C), implying the reaction between SiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> to form mullite. Mullite has very low dielectric loss and does not absorb microwave energy. Such a result can be well proved from the XRD detection shown in Fig. 2. It is obvious that mullite phase appears in the samples sintered at 1200 °C for 20 min. The

reflected power decreases at about 78 min (~1330 °C). This might be attributed to local fusion of SiO<sub>2</sub>. The successive decrease in reflected power after 123 min (~1550 °C) indicates the decomposition of mullite into Al<sub>2</sub>O<sub>3</sub> and SiO<sub>2</sub> [33].

Figure 3 shows XRD patterns of the SiC/Al<sub>2</sub>O<sub>3</sub> samples prepared at different temperatures. It is obvious that SiC, SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub> and mullite co-exist below 1450 °C. As the sintering temperature rises, local hot spot effect is enhanced. More mullite is formed around SiC particles. The peak height referring to mullite increases versus sintering temperature. Maximum amount of mullite appears at 1500 °C. At higher temperature, mullite tends to decompose readily due to the high electro-magnetic field. As a result, the height of peaks referring to mullite decreases at 1550 °C. Further heating of the SiC/Al<sub>2</sub>O<sub>3</sub> composites at 1600 °C, most of mullite peaks disappear and the peaks of Al<sub>2</sub>O<sub>3</sub> phase increase significantly. Such a result is well in accordance with Fig. 1.

Figure 4 shows the SEM images of the fracture surface of the SiC/Al<sub>2</sub>O<sub>3</sub> composites prepared by microwave sintering at different temperature. Needle-like mullite is observed on the surface of SiC particles at 1350 °C, as shown in Fig. 4a, which proves the above-mentioned local hot spot effect. The local hot spot effect refers to that only SiC particles absorb microwave at initial heating stage and become hot. Surface temperature of SiC particles with SiO<sub>2</sub> coating is much higher than that of Al<sub>2</sub>O<sub>3</sub> particles. Therefore, reaction between SiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> only occurs locally near the surface of SiC particles. That is why needle-like mullite is formed. As the temperature increases, the local hot spot effect is enhanced. More mullite phase is generated

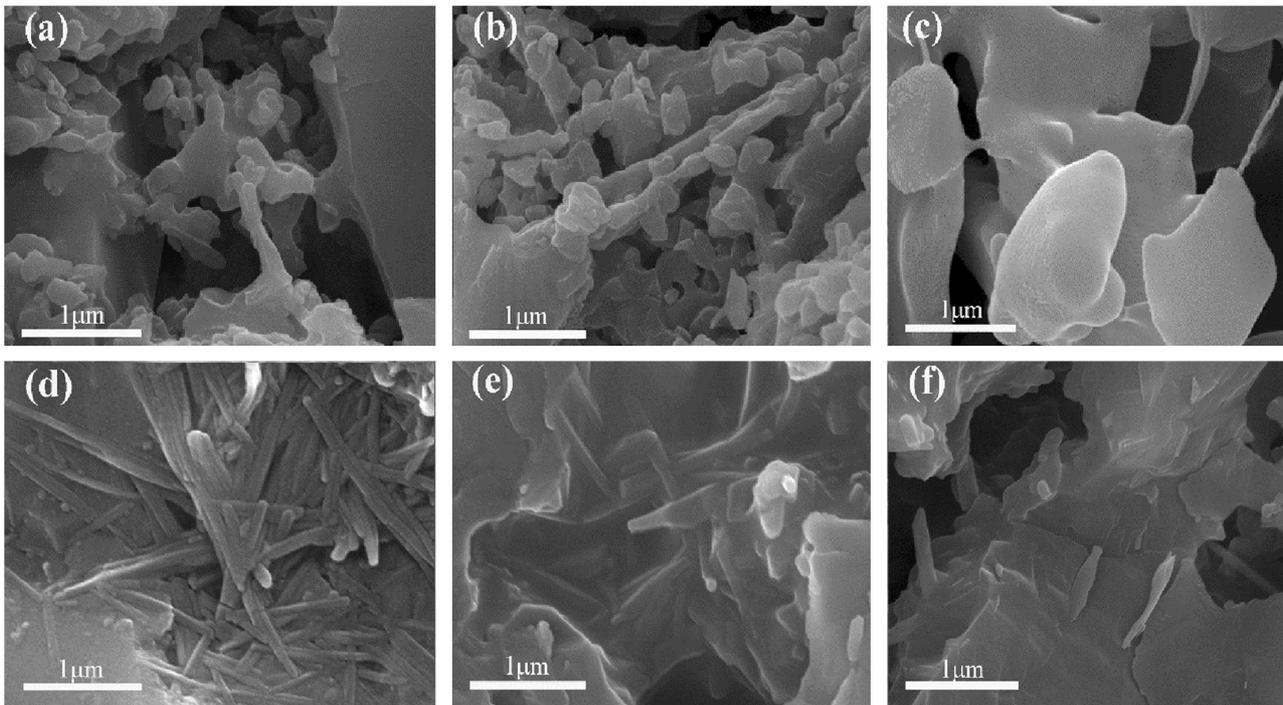


Figure 4. Fracture surface of SiC/Al<sub>2</sub>O<sub>3</sub> composites sintered by microwave at different temperatures: a) 1350 °C, b) 1400 °C, c) 1450 °C, d) 1500 °C, e) 1550 °C and f) 1600 °C

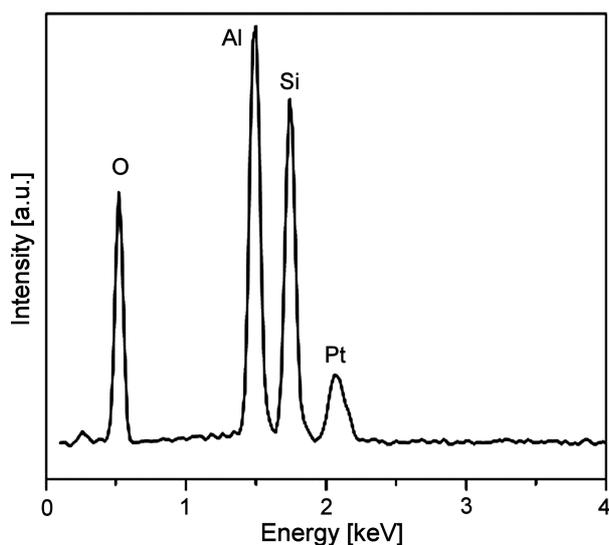
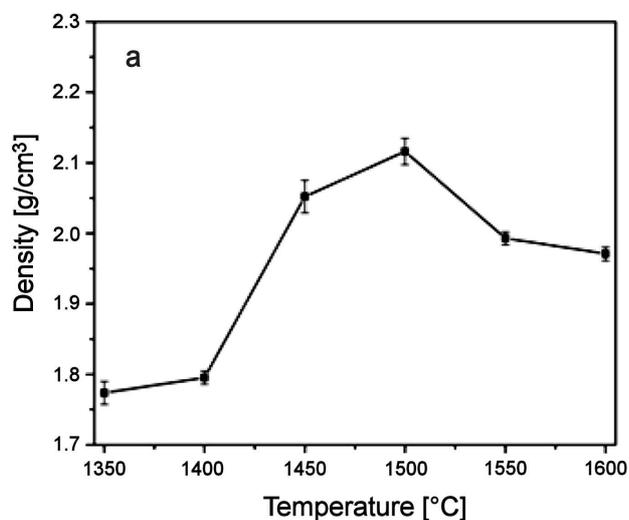


Figure 5. EDS spectrum of SiC/Al<sub>2</sub>O<sub>3</sub> composites sintered by microwave at 1450 °C (presented in Fig. 4c)

and growth of mullite is developed, as shown in Fig. 4b–d. Thus, higher amount of mullite appears within the samples prepared at 1400 °C. A mullite whisker bridge is observed between Al<sub>2</sub>O<sub>3</sub> and SiC particles at 1450 °C. The corresponding EDS spectrum, as shown in Fig. 5, indicates that the whiskers are composed of Al, Si and O elements. The distinctive bridging phenomenon of mullite whisker is the unique feature for microwave sintering related to the local hot spot effect. Massive well-grown mullite whiskers exist within the samples prepared at 1500 °C. Less mullite is observed within the samples prepared at 1550 °C due to its decomposition, as shown in Fig. 4e. Decomposition is enhanced at even higher temperature. As a result, most of mullite whiskers disappear within the samples prepared at 1600 °C.

Figure 6 shows the density and fracture toughness of SiC/Al<sub>2</sub>O<sub>3</sub> composites sintered by microwave at different temperatures. It can be seen that, the density and



fracture toughness increased with the increase of sintering temperature from 1350 °C to 1500 °C, the maximum density is 2.13 g/cm<sup>3</sup>, and the highest fracture toughness value of the SiC/Al<sub>2</sub>O<sub>3</sub> composites is 2.36 MPa·m<sup>1/2</sup>. Combined with the XRD and SEM analysis, we can find that the mechanical properties of mullite whiskers reinforced SiC/Al<sub>2</sub>O<sub>3</sub> composites are much better than the SiC/Al<sub>2</sub>O<sub>3</sub> composites without mullite whiskers.

#### IV. Conclusions

Mullite whiskers reinforced SiC/Al<sub>2</sub>O<sub>3</sub> composites were prepared by hybrid microwave sintering. The heating rate was well controlled by adjusting the input power. Mullite whiskers could be formed during microwave sintering. The local hot spot effect is the unique heating feature for microwave sintering which facilitates the directional growth of mullite whiskers bridging between SiC and Al<sub>2</sub>O<sub>3</sub> particles. The optimized microwave sintering temperature was 1500 °C corresponding to the maximum amount of mullite within SiC/Al<sub>2</sub>O<sub>3</sub> composites. Mullite decomposes to SiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> due to the high electro-magnetic field at higher temperatures, above 1550 °C. The mechanical properties of the mullite whiskers reinforced SiC/Al<sub>2</sub>O<sub>3</sub> composites are much better than the SiC/Al<sub>2</sub>O<sub>3</sub> composites without mullite whiskers.

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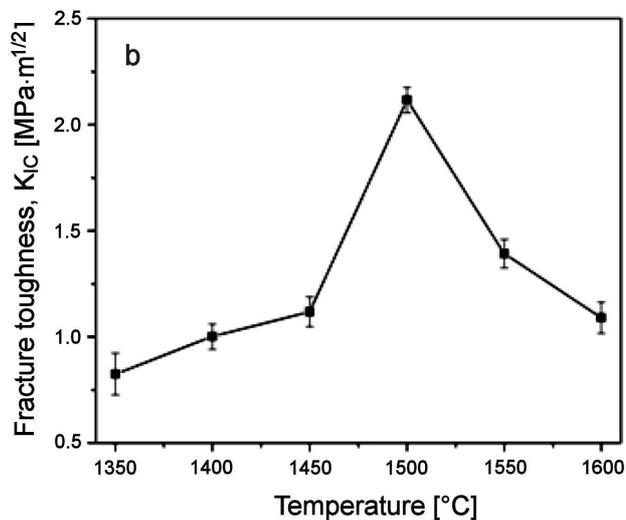


Figure 6. Density (a) and fracture toughness (b) of SiC/Al<sub>2</sub>O<sub>3</sub> composites

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